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Real-time characteristics of tidal bore propagation in the Qiantang River Estuary, China, recorded by marine radar



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ABSTRACT

Quantitative real-time observations of a tidal bore in a macro-tidal estuary are difficult and dangerous, particularly in large estuaries. Mathematical and numerical models have been used to predict tidal bore advances; however, to date, there have been no validations of large-scale flow patterns. A marine radar can provide valuable real-time information on tidal bore propagation. In this paper, a template matching method using a crosscorrelation algorithm was explored to estimate the evolution and celerity of a tidal bore with medium resolution marine radar images. The Qiantang River tidal bore was recorded at two different geographical locations. Characteristic flow patterns were derived and analysed, including temporal changes over a relatively large-scale area. The experimental results showed that the radar-derived celerity and calculated height of the tidal bore were consistent with visual observations in this estuarine zone.

1. Introduction

In an estuarine system, a tidal bore may form at the leading edge of flood tides, propagating upstream during the early flood tide (Tricker, 1965; Wolanski et al., 2004; Chanson, 2012). A tidal bore constitutes hydrodynamic discontinuity in terms of the pressure and velocity fields. Two types of tidal bores may be observed in nature, undular bores and breaking bores, based on their free-surface shapes (Chanson, 2010; Dolgopolova, 2013; Li et al., 2017). The former is characterised by a train of secondary waves following the non-breaking surge front (Peregrine, 1966). The latter presents a sharp discontinuity in freesurface elevation, with a rush and a roar, in the shape of a breaking roller (Lubin et al., 2010; Chanson, 2016). It is estimated that more than 400 estuaries worldwide are affected by tidal bores (Chanson, 2011, 2012). Although field observations of tidal bores have been conducted recently (Chanson, 2016; Chanson et al., 2011; Reungoat et al., 2015, 2017, 2018), there have been relatively few quantitative field studies of large tidal bores.

The Qiantang River tidal bore is a geophysical feature in China (Brownlie, 1901; Dai and Zhou, 1987). This tidal bore has been documented scientifically for nearly 2000 years (Cartwright, 2000; Krehl, 2009). Pertinent accounts include those of Wang (1962), Shi (1252), Moore (1888) and the Whangpoo Conservancy Board (1921) and, more recently, have included those of Zhu et al. (2012), Xie and Pan (2013),

Xu et al. (2016) and Chanson (2016). Fig. 1 presents the Qiantang River estuary. This estuary is a macro-tidal estuary with a funnel shape; its width decreases from the mouth in an upstream direction. The Qiantang River tidal bore results from the funnelling of the flood tidal wave into Hangzhou Bay (Chen et al., 1990; Madsen et al., 2005; Fan et al., 2012, 2014). Its upstream propagation takes place at a long distance, exceeding 100 km; numerous tidal bore warning signs have been erected on the river banks because of human deaths due to drowning in the bore (Pan and Chanson, 2015; Reungoat et al., 2018; Wang et al., 2019).

In recent years, marine radar technology has been widely used as a remote sensing tool for monitoring ships and sea conditions in coastal areas (Bell, 1999; Marmorino et al., 2004; Bell and Osler, 2011; Kokkini et al., 2017; Zervakis et al., 2017). Observations of internal waves using radar have been undertaken in the South China Sea (Huang et al., 2016; Zhang et al., 2016), but no studies of tidal bores based on marine radar have been published. We report herein on the propagation of the Qiantang River tidal bore, recorded by marine radar. This study develops a method to quantify the propagation of the tidal bore using medium resolution radar images. Following the introduction in Section 1, the data capture system and the image matching by cross-correlation are described in Section 2. The results concerning the evolution and celerity of the tidal bore are presented in Section 3. A discussion and summary of the results are presented in Sections 4 and 5, respectively.

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Fig. 1. Details of the Qiantang River Estuary, China. (a) Location of the Qiantang River Estuary in China; (b) Two radar test locations in the Qiantang River Estuary; (c) Test sites of R1-Yanguan and R2-Linhaicun, inset: radar vehicle.

2. Materials and methods

2.1. Radar data capture system

The radar data was collected with a system located at Yanguan (R1 in Figs. 1c and 30°24′08.55″N and 120°33′07.08″E) and Linhaicun (R2 in Figs. 1c and 30°22′59.77″N and 120°43′21.11″E) in the Qiantang River Estuary. A 6.5 foot (2.04 m) long radar antenna was mounted on the roof of a non-moving vehicle (see inset of Fig. 1c) and radar data acquisition tools were installed inside the vehicle. The system was based on a Furuno FAR-2127 marine radar employing 25-kW peak-power magnetron transmitters producing a beam width of 1.23° in a horizontal and 20° of a vertical plane, resulting in a range resolution of approximate 10 m over the scanned area with radius of 5 km. The antenna rotated at 42 rotations per minute (rpm), providing a revisit time of 1.429 s. The field observations were undertaken on 13 November 2015 at R1 with radar scan radius of 5 km and on 14 November 2015 at R2 with radar scan radius of 10 km. Table 1 summarises the operating

Table 1

Pa	rameters	of	the	radar	system	used	in	the	Qiantang	River	Estuary	•
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System parameter	Value
Peak output power	25 kW
Antenna type	2040 mm Open (6.5')
Frequency	9410 ± 30 MHz (X-band)
Beam Width (Horizontal)	1.23°(6.5' Open: XN-20AF)
Beam Width (Vertical)	20°
Range Scales	0.125–96 nm
Antenna Rotation Speed	42 rpm
Temperature	Antenna: 25 °C to + 55 °C; others: 15 °C to + 55 °C
Waterproofing	Processor unit: IPX0; Antenna unit: IPX6

parameters of the radar.

2.2. Template matching using a cross-correlation algorithm

The data were analysed to determine the celerity (phase velocity) vectors of the front of the tidal bore and to obtain potentially real-time information on the bore propagation. A cross-correlation algorithm was used to estimate spatial displacements (Δx , Δy) during a small increment of time Δt of 5.716 s (4 times the rotation period of radar antenna). Lengthways and transverse celerity magnitudes were calculated as *u* and *v*, respectively, as follows:

$$u = \frac{\Delta x}{\Delta t}, \ v = \frac{\Delta y}{\Delta t},\tag{1}$$

In the matching algorithm, image-patches of pixels from a set of paired radar images are compared and matched. Fig. 2 shows the matching concept and illustrates some commonly used terms, such as the template (*T*) that is the image-patch as a small portion of a reference image (Fig. 2a); the search window refer to the search space within which we are hoping to find out a match to the template in a paired image (Fig. 2b); and the subimage (*S*) is the overlapped area when the template (*T*) moves in the search window of pixel size $N \times N$. The cross-correlation coefficient between two image-patches *T* and *S* of pixel size $M \times M$ is defined by

$$R(i,j) = \frac{\sum_{m=1}^{M} \sum_{n=1}^{M} S^{i,j}(m,n) \times T(m,n)}{\sqrt{\sum_{m=1}^{M} \sum_{n=1}^{M} \left[S^{i,j}(m,n)\right]^2} \sqrt{\sum_{m=1}^{M} \sum_{n=1}^{M} \left[T(m,n)\right]^2}}$$
(2)

where *i*, *j* are the coordinates of the upper left corner in the subimage (*S*). Among all the computed R(i, j), the one with the largest value shows the cross-correlation coefficient for the best match, and $S_{i,j}$ is the



Fig. 2. Sketch map of tidal bore radar image template matching concept. (a) Template in a reference radar image; (b) Search window and subimage in a paired radar image.

match of *T*, which has been shifted by Δx in the *x* direction and by Δy in the *y* direction. The same procedure is repeated for other template in the reference image. This calculation yielded the bore celerity vector along the bore front in a manner comparable to that of Particle Tracking Velocimetry (PTV) (Fujita et al., 1998; Jodeau et al., 2008; Muste et al., 2008; Aberle et al., 2017).

2.3. Additional hydrodynamic and topographic data

To describe the hydrodynamic conditions of this study area, we considered the records of Yanguan Qiantang Bore Observation Station located 75 m upstream from R1 (see Fig. 3). This station has been operating since 2015 and performed recordings of tide level, discharge, current velocity and direction, suspended sediment concentration, pressures induced by the tidal bore on seawall and pier.

Three regular bathymetry surveys were carried out by the Zhejiang Surveying Institute of Estuary and Coast, China, in March, July and October 2015 (see Fig. 4). An echo sounder manufactured by Odom Hydrographic Systems, Inc., USA, was used to measure the water depths and a Real-Time Kinematic Global Positioning Satellite (RTK-GPS) system was employed to determine the locations. The sounding datum refereed to the level of lowest astronomical tide and the elevation used the 1985 National Vertical Datum of China. The survey in October 2015 was closer in time to the in-situ radar observations studied here. The water depth values mentioned later were derived from this survey.

The topographic distributions of sandbars and main channels varied dramatically between the three surveys. During the flood season from March to July, the scouring of main channel increased and deposition on the sandbar decreased. The main channel widened, while the elevation of sandbars tended to decrease. It was a contrary situation during the dry season from October to March. From July to October, the freshwater runoff weakened gradually and the tidal current increased firstly, reaching a maximum in September and then decreased. The significant difference in range of sandbars and main channels in the surveys emphasises the dynamic characteristics of the bathymetry in this area. This morphodynamic evolution may play an important role in tidal bore propagation and evolution (Chanson, 2012). The flow direction of the three main flood currents along the bank are basically marked as A, B and C in Fig. 4. The two main currents A and B were firstly separated by central sandbar then converged on the upstream side of R2, formed a single main current C and advanced forward.

3. Results

3.1. River conditions

The tidal bore was observed at two different locations (Fig. 1c), Yanguan (R1) and Linhaicun (R2), where the bore shape and pattern were substantially different. At Yanguan (R1), the bore is called the "Silk Bore" because the shape of the leading front looks similar to a silk thread. At Yanguan, the main channel of the river leans close to the north bank, and the width of the river is approximately 2.7 km. Before the arrival of the tidal bore on 13 November 2015, the mean water depth was 1.8 m, the average river flow velocity at the surface was 2.0 m/s, and the average height of the tidal bore was 1.4 m.

Linhaicun (R2) is a location where the two branches of the tidal



Fig. 3. Photos of observation station and tidal bore. (a) Yanguan Qiantang Bore Observation Station; (b) Incoming tidal bore at site R1.



Fig. 4. Survey data in (a) April 2015, (b) July 2015 and (c) November 2015, showing the significant changes of bathymetry in the study area. Red dashed arrows basically represent the flood tidal flow direction of the three main currents along the bank. (For interpretation of the references to colour in this figure legend, the reader is referred to the Web version of this article.)

bore meet, i.e., a "tidal bore crossing", and where the northern seawall is affected by large loads during bore impact. This bore encounter is called the "Crossing Bore". In the measurement area, the mean width of the river was 6.8 km. Before the bore arrival on 14 November 2015, the mean water depth was 1.6 m, and the average flow velocity at the surface was 1.0 m/s, while the average height of the tidal bore was 1.3 m. The mean water depth, the average flow velocity and the height of the tidal bore at the channel near the south bank were larger than those at the channel near the north bank.

3.2. Evolution of the tidal bore

The analysis of the tidal bore evolution was based upon the measurements of the positions of bore front for each radar image. The first step in detecting the bore front was to convert RGB (Red, Green, and Blue) images to grayscale by eliminating the hue and saturation information while retaining the luminance. Then, a reference image without tidal bore (Fig. 5a and b) was subtracted from each paired image to form a differential image. These difference images (Fig. 5c and d) separated tidal bore propagation from other bright but unchanged pixels, such as seawall, groyne and channel bank. Next, an algorithm was developed to detect the significant bright points though a thresholding operation and finally a line of best fit with these points can be determined as the front trajectory of tidal bore by the method of least squares.

Based upon the radar images, the front of the tidal bore propagating at Yanguan (R1) is shown in Fig. 6a. In the deep channel near the northern bank (depicted at the top of Fig. 6a), the front of the tidal bore was nearly perpendicular to the isobaths. In the shoal area, the intersection angles between the front of the tidal bore and the isobaths



Fig. 5. Front trajectories of tidal bore detecting concept. A reference image without tidal bore (a) at R1 and (b) at R2. A differential image (c) at R1 and (d) at R2. Yellow cross points represent detected bright points. A line of best fit with these points can be determined as the front trajectory of tidal bore. (For interpretation of the references to colour in this figure legend, the reader is referred to the Web version of this article.)

decreased with decreasing water depth. With the transverse variation in bathymetry linked to the deep channel, an *S*-shaped bore front curve was seen (Fig. 6b). Cross-waves were observed at locations where the bore front shape sharply changed (Fig. 6c). The cross-waves are shown in Fig. 6a with green lines.

Based upon the radar image analyses, the time-evolution of the tidal bore front at Linhaicun (R2) is presented in Fig. 7a. The two branches of the tidal bore advanced in different directions linked to varying river channel alignment. The bore front is marked in yellow and green in Fig. 7a. One bore, called the South Bore, propagated from south to north (Fig. 7b). Another bore, called the East Bore, propagated along the northern bank from east to west (Fig. 7c). Later, the two branches of the bore met next to the northern bank, i.e., the Crossing Bore (Fig. 7d). Finally, the South Bore impacted on the northern seawall, splashing over the seawall with waters rising as high as 10 m (Fig. 7e). In the deep channels near the banks, the fronts of the South and East Bores were also nearly perpendicular to the isobaths (Fig. 7a). The front of the South Bore was shaped in a corrugated pattern. In contrast, the front curves of the East Bore were relatively shorter and straighter than those of the South Bore. Fig. 7f illustrates a sequence of tidal bore fronts retrieved from marine radar data in 5-marine radar image intervals from t = 1200 s to t = 1300 s. They show that the two bores first encountered at t = 1221 s. After that, the East Bore became weak and gradually ceased to be observable. From the medium resolution radar images with a resolution of 20 m, the whole encounter process lasted for more than a minute.

3.3. Celerity of the tidal bore

A key feature of a tidal bore is its celerity or propagation speed. While the mean celerity may be derived analytically for simplistic boundary conditions (Tricker, 1965; Peregrine, 1966; Chanson, 2011), both field and laboratory observations have shown that the bore celerity fluctuates rapidly with time and space, even in simple geometry (Leng and Chanson, 2015a; Wang et al., 2017). Calculations in complex natural systems are far from trivial (Chanson, 2012), especially for accurate predictions and early warning. However, the rapid time and spatial fluctuations are rarely taken into consideration (Leng and Chanson, 2015b).

The results of the tidal bore celerity analysis at Yanguan (R1) are presented in Fig. 8a. In Fig. 8a, the black and blue arrows represent the fronts and cross-waves of the tidal bore, respectively. Neglecting local sharp fluctuations, the main tidal bore celerity contours are shown in 0.3 m/s intervals. Overall, the tidal bore celerity ranged between 5.4 m/sand 7.3 m/s, with a mean value of approximately 6.1 m/s. The crosswave celerity spanned between 6.4 m/s and 8.2 m/s, with a mean celerity of 7.5 m/s. The celerity of the tidal bore was faster along the southern bank than that along the northern bank. In fact, the average celerity along the northern bank was 5.2 m/s, and the average celerity along the southern bank was 6.5 m/s.

Fig. 8b shows the data in terms of the tidal bore celerity at Linhaicun (R2). In Fig. 8b, the black and blue arrows represent the fronts of the South Bore and the East Bore, respectively. The main celerity contours are presented in 0.6 m/s intervals. Overall, the South Bore propagated faster than the East Bore. The South Bore celerity was between 5.1 m/s and 8.2 m/s, with a mean value of 6.9 m/s. The East Bore celerity ranged between 4.6 m/s and 5.5 m/s, with a mean of approximately 5.0 m/s. Variation in both celerity magnitude and direction might be due to the locally varying bottom topography.

4. Discussion

Groyne

Seawal

Seawall

4.1. Comparison with visual observations

This study used radar images to derive the time evolution of freesurface flow patterns of a large tidal bore, delivering a large-scale view in a macro-tidal estuary. For safety, a security video monitoring system, called Mega Eyes (Fig. 9a), has been installed on the seawall of



Fig. 6. Tidal bore propagation at Yanguan (R1) on 13 November 2015. (a) The front (in yellow) of the tidal bore propagating at Yanguan detailing water depth (in grey-scale map with blue isobaths). The development of cross-waves (in green) observed at the location where the shape of the front sharply changed. (b) Tidal bore observed at the seawall of Yanguan. (c) Tidal bore observed at the opposite bank of Yanguan. (For interpretation of the references to colour in this figure legend, the reader is referred to the Web version of this article.)

Qiantang River. The installation locations are shown in Fig. 9d for the study area. This mature technology has been used to visually observe tidal bores in Qiantang River Estuary for over 10 years. The arrival time and height of the tidal bore were interpreted based on these observations combined with water gauge data (Fig. 9f).

The comparative results between visual observations and radarderived outcomes are shown in Table 2. The average celerity of the tidal bore from Xilongtou to R1 on 13 November 2015 was 5.3 m/s. This result was very similar to the radar-derived average celerity along the northern bank, near R1, of 5.2 m/s. The average celerity of the tidal bore from R2 to Xincang on 14 November 2015 was 5.5 m/s. The radarderived average celerity along the northern bank, near R2, was 5.0 m/s.

Although there were few data compared with visual observations, the feasibility and accuracy of the tidal bore information derived from marine radar image sequences, as a relatively novel technology, were in relatively good agreement with the visual observations extracted from the Mega Eyes system.

4.2. Approximate calculation of the tidal bore height

Considering tidal bore progression through an estuary, the motion of the bore front can be analysed as a quasi-steady hydraulic jump in translation, travelling from a downstream to an upstream direction with celerity C (Fig. 10). The integral forms of the mass and momentum conservation equations provide a series of relationships between the flow properties preceding and following the bore front (Chanson, 2011):

$$(V_1 + C)d_1 = (V_2 + C)d_2$$
(3)

$$\frac{1}{2}\rho g(d_2^2 - d_1^2) = \rho(V_1 + C)d_1(V_1 - V_2)$$
(4)

where *V* is the cross-sectional average flow velocity, *d* is the water depth, ρ is the water density, *g* is the gravity acceleration, and the subscripts 1 and 2 refer to the flow conditions at sections 1 and 2, i.e., before and immediately after the bore front. The solution to Equations (3) and (4) yields the height of the tidal bore *H*:

$$H = \frac{d_1}{2}(\sqrt{1+8Fr^2} - 3) \tag{5}$$

with the bore Froude number Fr defined as:

$$Fr = \frac{V_1 + C}{\sqrt{gd_1}} \tag{6}$$

and $H = d_2 \cdot d_1$.



Fig. 7. Tidal bore propagation at Linhaicun (R2) on 14 November 2015. (a) Two branches of tidal bores propagating at Linhaicun (water depth in grey-scale map with blue isobaths). The front is illustrated in yellow (the South Bore) from south to north; the green (the East Bore) propagating along the bank from east to west; two branches of the tidal bore encountered near the north bank (the Cross Bore). (b) South Bore propagation from south to north. (c) East Bore propagation from east to west. (d) Cross Bore near the north bank. (e) South Bore splashed over the bank with water rising higher than 10 m. (f) The two-bore encounter observed from radar data in 5-marine radar image intervals during a 100-s period. (For interpretation of the references to colour in this figure legend, the reader is referred to the Web version of this article.)

The Qiantang River tidal bore celerity *C* ranged from 4 to 10 m/s, which is 5–10 times larger than the initial cross-sectional average flow velocity V_1 in the first approximation, $V_1 = Q_1/A_1$, where Q_1 is the freshwater runoff and A_1 is the initial flow cross-section area. We used the records of Yanguan Qiantang Bore Observation Station and the bathymetric survey of in October 2015. The estimated initial cross-sectional average flow velocity was 0.6–0.8 times the flow velocity at the surface. The initial cross-sectional average flow velocity near R1 and R2 were 1.2 m/s and 0.6 m/s, respectively.

Based on the bathymetric survey of the estuary, the height of the bore was estimated from Equation (5) using the observed water depth, the bore celerity derived from the marine radar images and the initial cross-sectional average flow velocity. Fig. 11 presents the bore height *H* results along the investigated areas. Although no quantitative direct comparison with in-situ data was available over such a large-scale area, the magnitude and trends of the tidal bore height at the two sites were consistent with those expected from both visual observations (Table 2) and depth-averaged numerical calculations (Pan et al., 2007; Pan and Huang, 2010; Wang and Pan, 2018) for these estuarine areas. The data suggested that the tidal bore height tended to decrease with increasing water depth in the main channel near the bank of the Qiantang River. In

the shoaling area, the tidal bore height, to some extent, increased with decreasing water depth. Additional research is necessary to provide a conclusive explanation for this phenomenon.

4.3. Errors from the performed analyses and application perspective

During the observation period, the minimum celerity of tidal bore in the study area was approximately 5 m/s. The resolution of radar images obtained at R1 and R2 is 10 m and 20 m respectively. Considering the accuracy requirement of analysis, the time interval of a set of paired images used for matching at R1 and R2 should be greater than 2 s and 4 s respectively. In the current study, a time interval of 4 times the rotation period of radar antenna, i.e., 5.716 s, was selected as described in Subsection 2.2. Thus, the small celerity features during this time interval are smoothed. The limitation of this analysis need to be fully studied and it may relate to the resolution of the radar images. Further works should examine the exact correspondence between radar imagederived celerity and other direct instrumented measurements.

In Section 4.2, it was shown that the water depth (bathymetry), bore height and celerity are interrelated in a first approximation. The bathymetry is very difficult to obtain, at a reasonable price, and is



Fig. 8. Tidal bore front celerity data and water depth (in grey-scale map). (a) Celerity (phase velocity) vectors (in black) of the tidal bore propagating at Yanguan (R1). The arrows refer to the direction of celerity. Blue arrows show the cross-wave celerity vectors. The celerity contours (dashed lines in red) are at 0.3 m/s intervals. (b) Celerity (phase velocity) vectors of the tidal bore propagating at Linhaicun (R2). The arrows refer to the direction of celerity. Blue arrows show the East Bore celerity vectors. Black arrows show the South Bore celerity vectors. The celerity contours (dashed lines in red) are at 0.6 m/s intervals. (For interpretation of the references to colour in this figure legend, the reader is referred to the Web version of this article.)

rarely done on a regular basis. Meanwhile, the estuary water surface could provide the raw data about bore height and celerity. Although the measurement of bore height is much more difficult to obtain over a large area, it is perhaps achievable with photogrammetry or radar in selected locations. Consequently, the water bathymetry could be potentially derived from the celerity and height of the tidal bore in an inverse analysis based on hydrodynamic analysis of a macro-tidal estuary, as is the case in wave field analysis (Bell, 1999).

5. Conclusions

Marine radar image sequences were recorded, processed and analysed to determine the evolution and celerity of a very-large tidal bore in a macro-tidal estuary. The results demonstrated that the radar-derived celerity and height of the tidal bore were consistent with visual observations. The radar-image data delivered further detailed insights into the temporal evolution of the tidal bore, including spatial variations, which to date have been rarely documented, while providing real-time data that could be used to ensure the safety of tidal bore watchers.

Further research should include the following topics: (1) the feasibility of the radar method in comparison with field results using other direct instrumented measurements; (2) a more efficient matching algorithm with high resolution radar images to improve the accuracy of inversion; (3) shallow water bathymetry estimates based on hydrodynamic analysis of a macro-tidal estuary. Further, quantitative realtime observations of large-scale hydrodynamic events such as tsunami spread and run-up, flood waves resulting from dam break, spillway gate malfunction and landslide are a challenging problem in terms of instrument application and direct measurements. The presented method based upon radar image analysis would seem to provide a useful technique to estimate characteristic flow patterns in real time during such natural disaster events.

Declarations of interest

None.



Fig. 9. Field observations with the Mega Eyes system. (a) Mega Eyes system; (b) camera; (c) Yanguan (R1); (d) Location diagram and water depth (in grey-scale map). (e) Xilongtou; (f) water gauge; (g) Xincang.

Table 2

Comparison between visual observations and radar-derived outcomes.

Location	Arrive time (h: min: s)	Height (VO) (m)	Height (RD) (m)	Distance (m)	Celerity* (VO) (m/s)	Celerity [#] (RD) (m/s)			
a. 13 November 2015									
Linhaicun (R2)	11:58:09	1.2	-	3050	5.8	-			
Xincang	12:06:54	1.5	-						
Xilongtou	12:26:44	1.2	1.1	5870	5.3	5.2			
Yanguan (R1)	12:45:16	1.4	1.2						
b. 14 November 2015									
Linhaicun (R2)	12:27:16	1.3	1.1	3050	5.5	5.0			
Xincang	12:36:32	1.6	1.3						
Xilongtou	12:56:49	1.0	-	5870	5.4	-			
Yanguan (R1)	13:15:06	1.5	-						

VO: visual observations; RD: radar-derived outcomes; Celerity*: equal to the distance travelled divided by the time; Celerity[#]: radar-derived average value along the bank.



Fig. 10. Definition sketch of a tidal bore propagating upstream.



Fig. 11. Contour plot of estimated tidal bore height (Units: m) and water depth (in grey-scale map). (a) Yanguan (R1); (b) Linhaicun (R2).

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Appendix A. Supplementary data

Supplementary data to this article can be found online at https://doi.org/10.1016/j.csr.2019.04.012.

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